

The influence of the interfacial properties of composite catalyst material on the photocatalytic conversion of TiO₂ layer silicates

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Abstract

Solid-gas and solid-liquid interfacial properties of titanium dioxide/layer silicate composite sorbents were studied by sorption experiments and the photocatalytic properties were also investigated.

The photocatalyst TiO₂ was prepared by the sol-gel method and the sol obtained was used for heterocoagulation of Na-montmorillonite at several different mass ratios, yielding supported photocatalysts of various compositions. The TiO₂ content of the samples ranged from 20 to 75 wt%. The specific surface areas of the samples, determined by nitrogen adsorption, ranged from 120 to 290 m²/g. The catalytic properties of TiO₂/montmorillonite composites were tested by photo-oxidation of dichloro acetic acid (DCA). The specific surface area and the porosity exert a major influence on the photocatalytic efficiency through the interfacial layer properties. The rate of photo-oxidation of DCA depends strongly on the surface accessibility of the intermediates and the specific surface area calculated from gas and liquid mixture adsorption data. The conversion data of DCA presented show that the photocatalytic efficiency of TiO₂ can depend significantly on the accessibility of different molecules to the TiO₂ nanocrystals embedded in the layer silicate support in confined space.

Keywords

adsorption · liquid mixtures · surface area · porosity · photocatalysis · confined space

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Introduction

The surface properties of solid support materials can strongly influence the interfacial processes at the solid-liquid interface. Catalytic processes occur in the interfacial region in a distance range of 1-2 nm from the solid support material, which means that the adsorption layer structure and composition can influence the rate of the catalytic processes.

We expect that the catalytic properties of layer silicate supported TiO₂ nanoparticles can be predicted from binary liquid adsorption isotherms. The surface of the layer silicate is hydrophilic, because the surface of the silicate layer has a negative charge, which is compensated by sodium cations. Incorporation of TiO₂ nanoparticles into the interlamellar space will modify the surface energy of the clay support material for adsorption processes.

Titanium dioxide is one of the most important photocatalysts, by virtue of its chemical stability and its good light absorption properties. Preparation of TiO₂ has been the subject of a large number of publications [1]-[8]. The majority of these works describes titanium dioxide products prepared by controlled hydrolysis of titanium(IV) alkoxides. In the course of hydrolysis, water is the reaction partner of the titanium precursor and, in most cases, it is also the main component of the reaction medium (alcohol/water mixture). In the various publications, the water content of the reaction medium varies over a wide range, from pure water to a water content corresponding to the stoichiometry of hydrolysis [9]-[16]. Many publications are found in the relevant literature on the preparation and evaluation of composite materials containing titanium dioxide. Supported or composite materials possess more advantageous properties for practical applications than pure titanium dioxide [9]-[12]. Among composite-forming or support materials with hydrophilic or hydrophobic surface characteristics, layer silicates are most widely used [16]-[18]. Sterte et al. performed acid hydrolysis of titanium(IV) chloride. The TiO₂ sol formed was added to montmorillonite suspensions [1]. The products exhibited very low crystallinity; the onset of anatase formation was detected by X-ray diffraction. Typically, the TiO₂ sol prepared under acidic conditions was added to suspensions of Na-montmorillonite and

the structure of the nanocomposite obtained was studied. In all cases highly acidic sol was used ($\text{pH} < 1.8$). The nanocomposites obtained contained amorphous or barely crystalline titanium dioxide. The anatase phase appeared only if the composites were subsequently heat-treated (by hydrothermal procedure or calcination). The pillars are very small, typically 1-2 nm. The extremely large specific surface areas (200-400 m^2/g), considerably reduced by heat treatment, are due to the amorphous structure and the very small particle size [14]-[18].

Photocatalytic oxidation of numerous compounds has been studied on titanium dioxide catalyst. Preferred model compounds have been phenol [18] and its chlorinated derivatives [6], salicylic acid and other carboxylic acid derivatives [19], dye molecules [10], and dichloroacetic acid [20]. Efforts have been made to optimize the accessible catalytic surface of supported and composite catalysts containing titanium dioxide.

The aim of the present work was to prepare, by heterocoagulation, pillared $\text{TiO}_2/\text{montmorillonite}$ nanocomposites for which the solid-gas and solid-liquid adsorption properties of the composite catalyst materials are known. Using different $\text{TiO}_2/\text{layer}$ silicate mass ratios, the structure of the composites can be modified systematically. The samples obtained by heterocoagulation, having different specific surface area and porosity and high crystalline anatase content, will be investigated in sorption and photocatalytical experiments.

1 Adsorption of binary liquid mixtures on solid surfaces

When solid particles are immersed in a liquid medium, solid/liquid interfacial interactions will cause the formation of an adsorption layer on their surface. Following D.H. Everett, G. Schay and L.G. Nagy, the sorption exchange process taking place at the solid-liquid interface may be described in thermodynamically exact terms when the activities of the interfacial layer and of the bulk phase are known. In accordance with the exchange equilibrium in binary liquid mixtures at the solid-liquid interface, the liquid sorption equilibrium constant (K) is given by the following formula [21]-[28]:

$$(1) + r(2)^s \rightleftharpoons (2)^s + r(1) \quad (1)$$

$$K = \frac{x_1^s f_1^s (x_2 f_2)^r}{(x_2^s f_2^s)^r x_1 f_1} \quad (2)$$

where x_1^s and x_2^s are the molar fraction of the interfacial layer and x_1 and x_2 that in the bulk liquid phase respectively, f_1^s and f_2^s are the activity coefficients in the interfacial layer and f_1 and f_2 in the bulk liquid. Assuming that $f_1^s/f_2^s \approx 1$, i.e., that the activity coefficients of the interfacial phase compensate for each other [29]-[31], then

$$K' = \frac{x_1^s (a_2)^r}{(x_2^s)^r a_1} \quad (3)$$

If the activity data of the bulk phase are known, the value of K' can be calculated at a given value of molecular exchange

ratio: $r = V_{m,2}/V_{m,1}$ by means of computer iteration [32]-[35]. The applicability of Eq. (3) has been investigated by I. Dékány et al. in several publications [32]-[36]. It is revealed by the adsorption equilibrium diagrams that when the adsorption of a liquid pair consists of components with significantly different polarities, the value of the equilibrium constant K' decreases with increasing surface hydrophobicity of the different silicate surfaces covered by alkyl chains [38]-[43].

The material content of the adsorption layer is the adsorption capacity of the solid adsorbent, which may be determined in binary liquid mixtures if the so-called adsorption excess isotherm is known. Owing to adsorption, the initial composition of the liquid mixture, x_1^0 , shifts to the equilibrium concentration x_1 , where $n^s = n_1^s + n_2^s$ is the mass content of the interfacial phase (e.g., mmol/g). The difference, $x_1^0 - x_1 = \Delta x_1$, can be determined by simple analytical methods. The relationship between the reduced adsorption excess amount calculated from the change in concentration, $n_1^{\sigma(n)} = n^0(x_1^0 - x_1)$ and the material content of the interfacial layer is given by the Ostwald-de-Izaguirre equation [21]-[25]. In the case of purely physical adsorption of binary mixtures, the material content of the adsorption layer ($n^s = n^0 - n$) for component 1 is illustrated by the following material balance [22]-[25]:

$$n^0 x_1^0 = n_1^s + (n^0 - n^s) x_1 \quad (4)$$

$$n_1^{\sigma} = n^0(x_1^0 - x_1) = n^0 \Delta x_1 \quad (i = 1, 2, \dots) \quad (5)$$

where n^0 is the total quantity of liquid mixture referred to unit mass of the adsorbent (e.g., mmole/g adsorbent), x_1^0 is the mole fraction of the i -th component before adsorption, and x_1 is that in the equilibrium homogeneous liquid phase. The adsorption excess isotherms $n_1^{\sigma} = f(x_i)$ calculated in accordance with Eq. 1 can be classified into five basic types by the Schay-Nagy isotherm classification [22]-[24]. The Ostwald-de Izaguirre equation is obtained, free of assumptions, from the mass balance:

$$n^0(x_1^0 - x_1) = n_1^{\sigma(n)} = n_1^s - n^s x_1 = n^s(x_1^s - x_1) \quad (6)$$

where $x_1^s = n_1^s/n^s$ is the mole fraction of the interfacial phase. According to Eq. (3), therefore, the excess isotherm $n_1^{\sigma(n)} = f(x_1)$ stems from a combination of the „individual” isotherms $n_1^s = f(x_1)$ and $n^s = f(x_1)$ [22]-[24].

Isotherms of types II, III and IV in the Schay-Nagy classification have the common characteristic that a fairly long section of the isotherm is practically linear [21-25]. For the linear section, we may write

$$n_1^{\sigma(n)} = a - b x_1 \quad (7)$$

Combining Eqs. (3) and (4):

$$a - b x_1 = n_1^s - n^s x_1 = n_1^s - (n_1^s + n_2^s) x_1 \quad (8)$$

Assuming that the intercepts of the linear sections are equal to the adsorption capacities of the components at the points $x_1 = 0$

and $x_2 = 1$, for the $x_1 = 0$ intercept $a = n_1^s$, while for the $x_2 = 1$ intercept $a - b = -n_2^s$ [21-25]. Since, in liquid sorption, the surface of the adsorbent is always completely covered, according to Williams the following equation can be written for the case of monomolecular surface coverage:

$$n_1^s a_{m,1} + n_2^s a_{m,2} = a_L^s \quad (9)$$

where $a_{m,1}$ and $a_{m,2}$ are the cross-sectional areas of the components 1 and 2, which can be calculated from the molar volumes of the components, and a_L^s is the equivalent specific surface area [29,31,42].

Eq. (6) can also be written in the following form:

$$n_1^s + r n_2^s = n_{m1,0}^s \quad (10)$$

where $n_{m1,0}^s$ is the monomolecular adsorption capacity of pure component 1, and

$$a_L^s = n_{m1,0}^s a_{m,1} \quad (11)$$

According to Eqs. (10) and (11), the specific surface area of the adsorbent can be calculated from a knowledge of the adsorption capacities and the cross-sectional areas. The above method for determining the specific surface area has been applied to many systems in the literature, and it has been found that the specific surface areas calculated with the Schay-Nagy extrapolation method for non-swelling and disaggregating adsorbents agree very well with those calculated by the B.E.T. method [21]-[25].

The adsorption capacity $n_{1,0}^s$ of the pure component can be determined by the Everett-Schay (ES) method [21]-[28], [31]-[37]:

$$\frac{x_1 x_2}{n_1^{\sigma(n)}} = \frac{1}{n_{1,0}^s} \left[\frac{r}{S-1} + \frac{S-r}{S-1} \right] x_1, \quad (12)$$

For ideal adsorption from ideal solutions, S is constant [21]-[25]. The constancy of the separation factor in many other cases may result from compensation effects. From the linear dependence of $x_1 x_2 / n_1^{\sigma(n)}$ on x_1 , we determine the value of $n_{1,0}^s$.

Given the knowledge of the adsorption excess isotherm $n_1^{\sigma(n)} = f(x_1)$, the so-called Individual isotherms are given by the following equations [21]-[25]:

$$n_1^s = \frac{r^* n_1^{\sigma(n)} + n_{1,0}^s x_1}{x_1 + r^* x_2} \quad (13)$$

$$n_2^s = \frac{n_{1,0}^s x_2 - n_1^{\sigma(n)}}{x_1 + r^* x_2} \quad (14)$$

where $n_{1,0}^s$ is the adsorption capacity relative to pure component 1 and $r^* = V_{m,2} / V_{m,1}$ is the ratio of the molar volumes of the components. In case of U-shaped excess isotherms, the adsorption capacity ($n_{1,0}^s$) can be determined from the linearized Everett-Schay function using Eq. (12) [21]-[25]. If the adsorption layer amount is known, the volume of the layer is obtained from the equation $V^s = n_{1,0}^s V_{m,1}$, and the volume fraction of

the adsorption layer can be calculated from the data of excess isotherms by the following equation:

$$\phi_1^s = \frac{n_1^s}{n_{1,0}^s} = \phi_1 + \frac{r^* n_1^{\sigma(n)} V_{m,1}}{V^s (x_1 + r^* x_2)} \quad (15)$$

If the specific surface area (a_L^s) of the particles is known, the thickness of the layer is $t^s = V^s / a^s$, which can be calculated from Eq. (15):

$$t^s = n_1^{\sigma(n)} \left(\frac{V_{m,1}}{a^s x_1} \right) \left[\frac{\phi_1}{\phi_1^s - \phi_1} \right] \quad (16)$$

where ϕ_1^s and ϕ_1 are the volume fractions of the adsorption layer and of the bulk phase, respectively, in adsorption equilibrium. The layer thickness t^s calculated according to the equation above is nearly constant. In non-ideal liquid mixtures, however, its value may depend on the composition of the bulk phase. In calculations of stability for disperse systems, knowledge of the thickness of the stabilizing adsorption layer is highly important [41]-[43].

2 Experimental

2.1 Materials

The TiO₂ nanoparticles were prepared using titanium(IV) isopropoxide (Fluka Chemica, pract.), purified water (Milli-Q, R = 18 MΩcm) and 2-propanol (Reanal Hungary, puriss). Concentrated hydrochloric acid (Reanal Hungary, pro anal.) and sodium hydroxide (Reanal Hungary, puriss) were used in the experiments. The TiO₂/clay mineral nanocomposites were prepared using Na-montmorillonite (EXM-838, D < 2 μm, Süd-Chemie AG, Germany) as support material. The liquid sorption measurements were made from ethanol-cyclohexane binary liquid mixtures. In the photocatalytic efficiency studies the photodegradation of dichloroacetic acid (DCA, Aldrich, 99+%) was monitored.

2.2 Sample preparation

2.2.1 Preparation of the TiO₂ nanoparticles

The TiO₂ nanoparticles were prepared in aqueous media by means of sol-gel technique. A mixture of 174 mL titanium(IV) isopropoxide and 146 mL 2-propanol was added drop-wise into 660 mL Milli-Q water in 5 minutes under vigorous stirring in N₂ atmosphere. Due to hydrolysis a white, colloidal dispersion was formed, followed by the addition of 18 mL concentrated hydrochloric acid to the white slurry (pH ~ 1). The product was held under thermostatic conditions (t = 50 °C) for 12 hours. After the hydrothermal treatment an almost transparent, stable Ti(OH)₄/TiO₂ sol was obtained.

2.2.2 Preparation of the Ti(OH)₄-TiO₂/layer silicate nanocomposites

The original pH of the Ti(OH)₄/TiO₂ colloidal sol was around pH = 1. The calculated amount of the sol was added into the 1 % (g clay/100 mL of water) Na-montmorillonite suspension under vigorous stirring in 30 minutes. Different TiO₂/clay mass

ratios were used resulting in different compositions of the photocatalysts. The theoretical added TiO₂ contents were 20, 33, 50, 66, 75 w%. After 20 hours sedimentation, the heterocoagulated Ti(OH)₄-TiO₂/Na-montmorillonite precipitates were centrifuged at 10000 rpm for 30 minutes followed by washing of the solid phase using Milli-Q water. The twice-washed product was re-dispersed in Milli-Q water and the suspension was dialyzed for 90 hours to remove the residual electrolyte from the liquid phase. The dialyzed suspension was centrifuged again, and the solid phase was collected then dried at 50 °C in a hot box oven. These nanocomposite samples have the following notation: e.g., TiO₂ 75/MA, where “75” means the semiconductor content of the nanocomposite in weight % units, “M” means the Na-montmorillonite support and “A” means the high acidic circumstances during preparation.

2.3 Measurement methods

The XRD experiments were carried out in a Philips X-ray diffractometer (PW 1930 generator, PW 1820 goniometer) with CuK- α radiation ($\lambda = 0.1542$ nm) 40 kV, 35 mA. The basal spacing (d_L) was calculated from the (001) reflection via the Bragg equation using the PW 1877 automated powder diffraction software.

Specific surface areas of TiO₂/Na-montmorillonite nanocomposites and TiO₂ samples were determined by a Micromeritics gas adsorption analyzer (Gemini Type 2375) at 77 K in liquid nitrogen. The adsorption and desorption branches of the isotherms were determined. Prior to measurements the samples were pre-treated in vacuum (ca. 0.01 torr) at 393 K for 2 hours. The sample holder was loaded with ca. 0.1-0.3 g of samples. The adsorption isotherms were analyzed by means of the BET equation, the micropore volume data were determined with the de Boer's t-method, and the pore size distribution curves were analyzed by the Barret-Joyner-Halenda (BJH) method [44]. To determine the adsorption excess isotherms at $25 \pm 0.1^\circ\text{C}$ a Zeiss differential interferometer was used and 0.1 g catalyst was dispersed in 5 ml liquid mixtures in the whole composition range. After establishment of the adsorption equilibrium (24 hours) the equilibrium composition was determined by interferometry and the excess isotherms were calculated from Eqs. (4-6).

For the band gap energy determination the optical properties of the composites were determined using an Ocean Optics Chem2000 diode array spectrophotometer.

The effective titanium content of the TiO₂ containing nanocomposites was determined by inductively coupled plasma (ICP) spectrometry using a Jobin-Yvon 24 sequential ICP-OES analyzer.

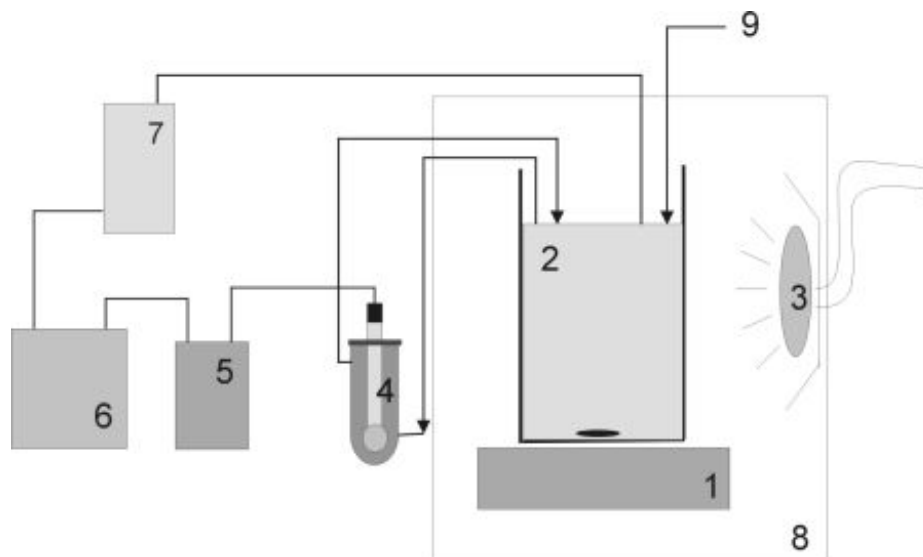
The photodegradation of the dichloroacetic acid, the model pollutant, was monitored by pH-stat titration. Constant ionic strength ($I = 10$ mmol/l, KNO₃) was used in all experiments. The reaction vessel was thermostated during the irradiation ($t = 25^\circ\text{C}$). All experiments were performed in 200 mL suspension in which the DCA concentration was 1 mmol/l. The ir-

radiation procedure was carried out in a home-built system and the reaction was controlled by home-written software. Photocatalytic experiments were carried out in a thermostated glass reactor equipped with an external pH measurement cell. The suspension was continuously circulated at a constant rate by means of a peristaltic pump. The instantaneous value of the pH of the suspension was measured on-line. The schematic diagram of the reactor is represented on the Fig. 1. The suspension of the DCA solution and the given catalyst were introduced into a glass reaction vessel (2), then transferred to a photoreactor box (8) equipped with a 150W high pressure mercury lamp (3). The suspension was stirred continuously using a magnetic stirrer (1). A small amount of the total volume of the suspension was continuously extracted and returned using a peristaltic pump (not shown in the diagram) into the external measuring cell (4) equipped with a combined pH-electrode. In all cases, air was introduced into the suspensions (9) at a constant flow rate (1 mL/min) during the illumination. The raw signal generated by the pH-electrode was converted by a D/A converter (5) and then processed by the PC (6), which controlled the automatic burette (7) by means of the home-made software noted in ref. [44].

3 Results and Discussion

3.1 Structural properties of TiO₂/layer silicate nanocomposites

X-ray diffractograms in the 2θ angle range $20\text{--}30^\circ$ characteristic of series M were taken after drying the samples at 50°C (Fig. 2). The reflections found in this range are characteristic of the structure of titanium dioxide. The peaks at 25.3° (2θ) and 27.5° (2θ) correspond to the anatase (101) and rutile (110) phases, respectively. The intensities of the reflections at 25.3° (2θ) increase with increasing TiO₂ content, demonstrating that, in the course of sol preparation, only the anatase crystalline modification of TiO₂ was formed, since the reflection characteristic of rutile ($2\theta=27.5^\circ$) is missing. For samples prepared by sol-gel synthesis the anatase reflection calculated from the Bragg equation is $d_{101} = 3.52$ Å, whereas the average particle diameter calculated from the half-width values of the same peaks by the Scherrer equation is 3.6-4.0 nm. The reflections seen in the small angle region of the diffractograms are characteristic of the silicate layer used as support, and their intensities decrease with increasing composite TiO₂ content. Basal spacings (d_L), calculated with the Bragg equation from the reflection characteristics of the intercalation structure in the small angle region ($1\text{--}15^\circ$ (2θ)), were found at $2\theta=2.5^\circ$ and are listed in Table 1. Based on these data, the average basal spacing values lie in the range of 3.4-3.6 nm. The particle diameter calculated using this value, $d_{\text{TiO}_2} = d_L - d_{\text{TOT}}$ (where $d_{\text{TOT}} = 0.96$ nm, i.e., the thickness of a single lamella of Na-montmorillonite generated by tetrahedral-octahedral-tetrahedral planes) is 2-3 nm.



(1: magnetic stirrer, 2: glass reaction vessel and suspension, 3: high-pressure mercury lamp, 4: external measuring cell with combined pH-electrode, 5: D/A converter, 6: computer, 7: automatic burette, 8: photoreactor box, 9: air inlet)

Fig. 1. Schematic arrangement of the measurement systems for photocatalytic reactions.

Tab. 1. Structural and optical properties of the photocatalyst samples

sample	(1)TiO ₂ content (%)	(2)d _L (nm)	(3)λ _g (nm)	(4)E _g (eV)
sol-gel TiO ₂	100	—	397	3.12
sol-gel TiO ₂ (400 °C)	100	—	477	2.60
TiO ₂ 75/MA	69.01	3.46	378	3.28
TiO ₂ 66/MA	63.51	3.48	377	3.29
TiO ₂ 50/MA	47.41	3.49	375	3.30
TiO ₂ 33/MA	29.42	3.50	373	3.32
TiO ₂ 20/MA	18.91	3.49	367	3.38
Na- montmo- rillonite	0	1.15	-	-

(1) TiO₂ content determined by ICP measurement

(2) Determined by XRD measurements and calculated from the Bragg equation

(3) Determined from absorbance measurement of the dilute (0.01-0.05 g/100 mL) suspensions

(4) Calculated by $\lambda_g = 1240/E_g$, where E_g is the band gap energy in eV units

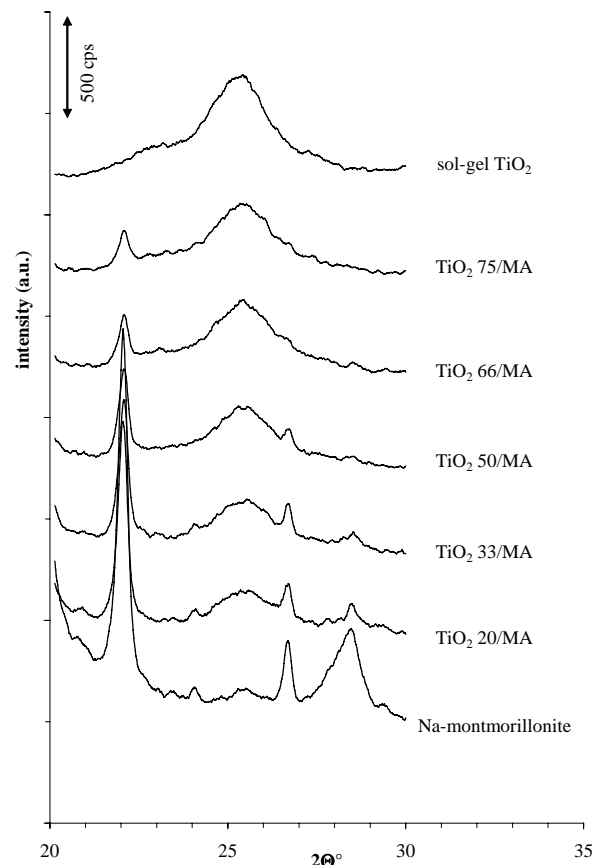


Fig. 2. XRD pattern of titanium-dioxide and in titania-intercalated montmorillonite.

The specific surface areas and the porosities of the samples were determined by N_2 adsorption measurements. Isotherms were analyzed by the BET method; the specific surface areas of the samples were determined and are listed in Table 2. The specific surface area of the original layer silicate used as support

(ca. 28 m²/g) increases gradually with increasing TiO₂ content, because TiO₂ particles are incorporated between the lamellae. It is also seen that pure TiO₂ prepared by the sol-gel method has a high specific surface area (ca. 270 m²/g). We suppose that the high specific surface area of composites is the cumulative

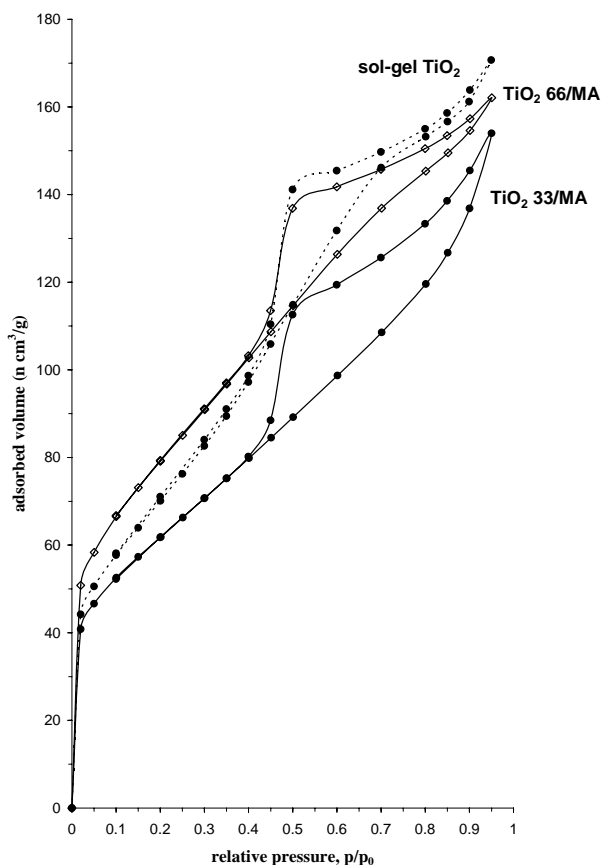


Fig. 3.a. Nitrogen adsorption isotherms at 77 K on different TiO₂-montmorillonite composites and the titania photocatalyst prepared by sol-gel method.

result of two effects. On the one hand, pillaring the lamellae of layer silicates generates a layered nanocomposite material with a larger internal surface; on the other hand, porous TiO₂ located in the interlamellar space also contributes to the increase in specific surface area. Based on previous results and experience, this increase in specific surface area can be attributed to a modification of the structure of the layer silicate support in the highly acidic medium due to dissolution of Al ions from the crystal lattice. Taking into consideration that particle synthesis itself takes place under extremely acidic conditions (pH < 1), it can be concluded that the increase in specific surface area is a result of the increase in the surface and porosity of the clay mineral [44]. Fig. 3.a shows some of the nitrogen adsorption isotherms at 77 K, namely the samples with 33%, 66% TiO₂ content and of sol-gel TiO₂. All three isotherms clearly belong to type IV of the classification according to Brunauer, Emmett and Teller (BET), characteristic of porous adsorbents [22,24]. The hysteresis loops indicate high porosity. It can be established on the basis of the shape of the hysteresis loop that in each sample the size distribution of pores is only slightly polydisperse. The pores in the samples fall into the range of micro- and mesopores. The pore size distribution was calculated from the appropriate section of the desorption branch of each isotherm using the Barrett, Joyner, Halenda (BJH) method [22,24,44]. In the case of the TiO₂/MA series, the maximum of the pore size distribution curve fluctuates

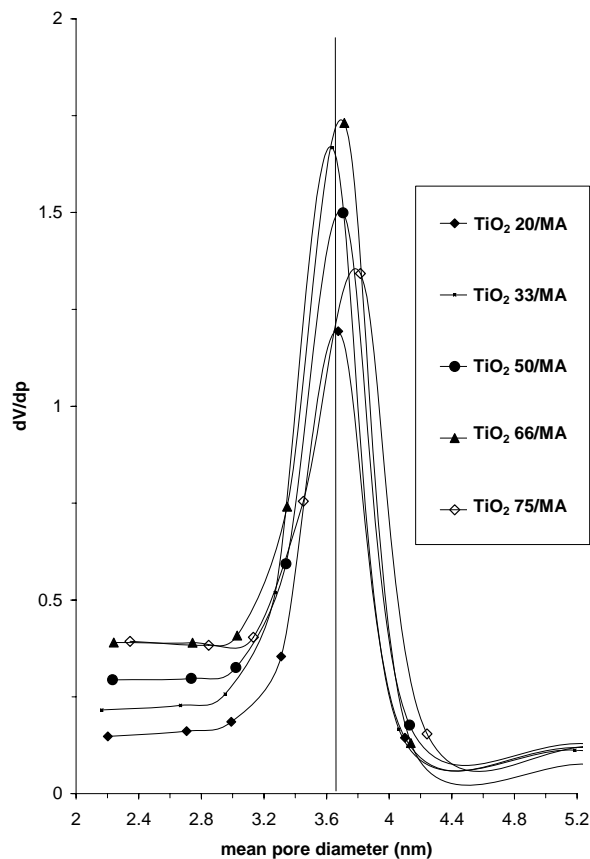


Fig. 3.b. Calculated pore size distribution functions using nitrogen adsorption measurements on different TiO₂-montmorillonite composites and the titania prepared by sol-gel method.

around a given value (3.6-3.7 nm) (see Fig. 3.b). The most characteristic pore diameters lay in the range 3-4 nm for both series. These data are in good agreement with the values of d_L measured by X-ray diffraction Table 1. The sol-gel TiO₂ sample also exhibits porous character: adsorption hysteresis is observed in its isotherm as well.

Tab. 2. Results of the nitrogen adsorption experiments

sample	(1) a_{BET}^S m ² /g	(2) a_{ext}^S m ² /g	(2) a_{mp}^S m ² /g	(2) V_{mp} cm ³ /g	(3) V_{max}^S cm ³ /g (STP)
Na-montmorillonite	28	41	6.3	0.0030	59.5
TiO ₂ 20/MA (50 °C)	153	143	9.49	0.0041	128.4
TiO ₂ 33/MA (50 °C)	198	193	4.66	0.0012	143.4
TiO ₂ 50/MA (50 °C)	240	—	—	—	157.3
TiO ₂ 66/MA (50 °C)	251	—	—	—	156.9
TiO ₂ 75/MA (50 °C)	270	—	—	—	176.6
sol-gel TiO ₂ (50 °C)	268	—	—	—	149.4

(1) calculated by the BET equation

(2) determined by the deBoer's t-plot method

(3) maximum adsorbed volume data is given in normal units of cm³/g

The adsorption isotherms belong to type II in the Schay-Nagy classification. That means the ethanol will be adsorbed preferentially on the polar surface of the composite adsorbent. The slopes of the isotherms depend on the TiO₂ content of the composite samples.

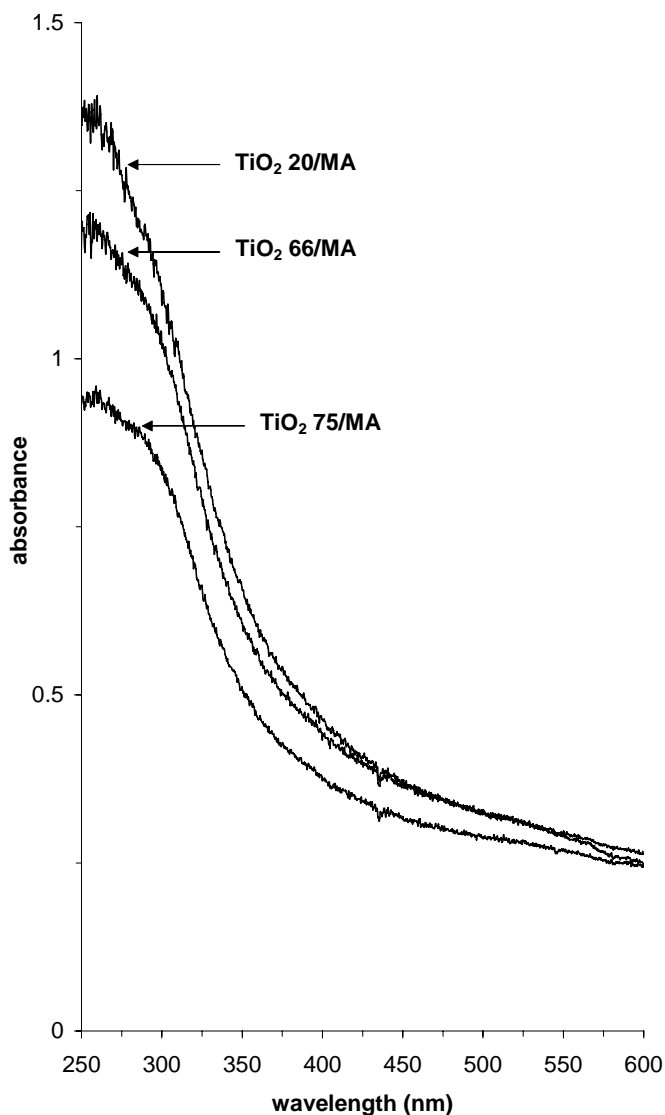


Fig. 4. UV-Vis absorption spectra of TiO₂-montmorillonite composites.

The calculated adsorption capacities, using Eqs. (7) and (12), agree well with each other. The specific surface area calculated from the N₂ adsorption data is nearly the same for the TiO₂ 66 MA sample. The TiO₂-montmorillonite composites show higher equivalent specific surface area at low TiO₂ content than the BET surface area, because it is possible to build up a second adsorption layer for ethanol in the confined space of the layer silicate support. If the TiO₂ content is higher, the liquid sorption capacity is lower, because the interlamellar free space between the TiO₂ pillars is also smaller. That means that ethanol does not have access between the layers, and only nitrogen molecules can be incorporated into the small pores. The average adsorption layer thickness ranges between 0.47 and 0.53 nm, showing the bilayer structure formation of ethanol in the interlamellar confined space as calculated from Eq. (16) (see Table 3).

The band gap energy (E_g , given in eV) of nanocomposites and pure sol-gel TiO₂ was determined on the basis of UV-Vis photometric assays in order to identify the wavelengths that can excite TiO₂/montmorillonite nanocomposites for the purposes of photocatalysis. Typical light absorption spectra of some nanocom-

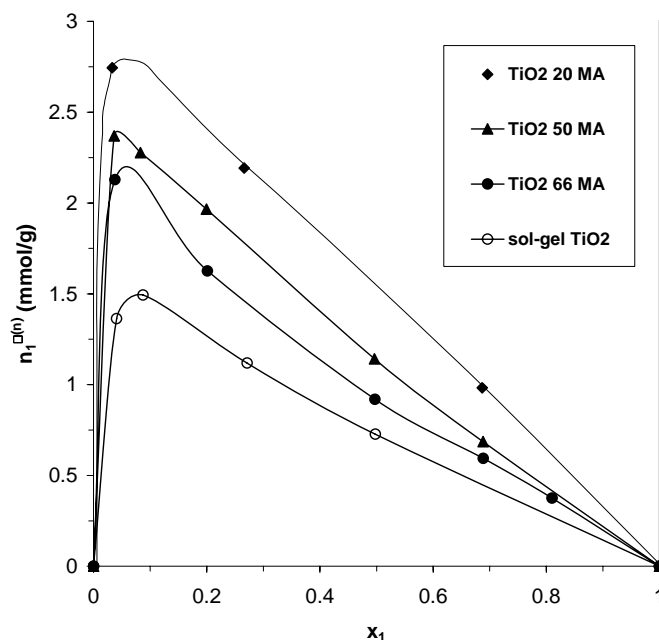


Fig. 5. Adsorption excess isotherms in ethanol(1)-cyclohexane(2) binary liquid mixtures on the different photocatalysts.

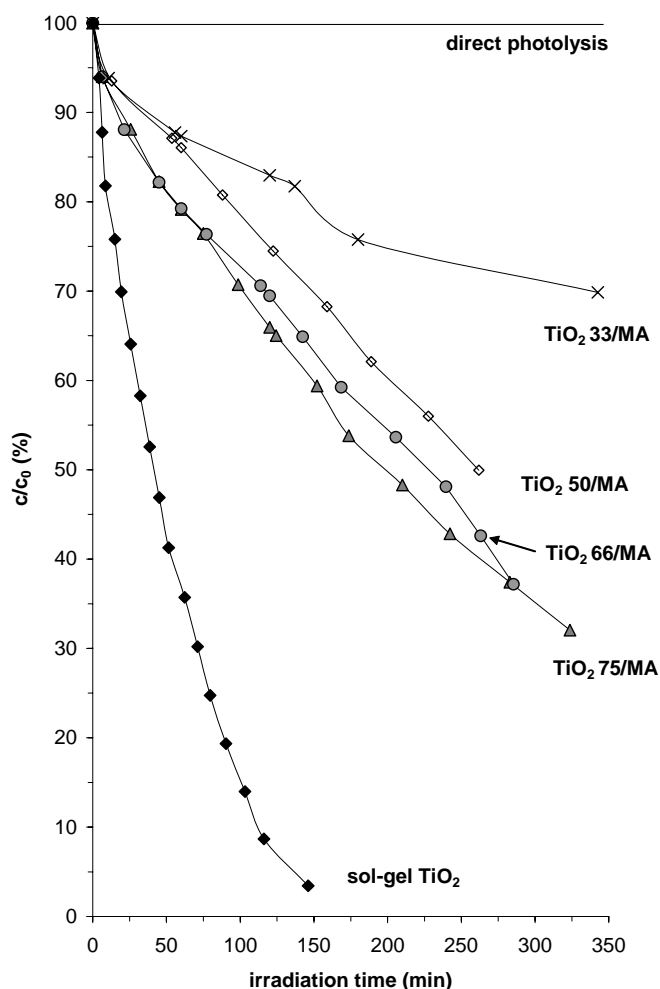


Fig. 6. Photo-oxidation process of DCA on different photocatalyst composites.

posites, which were used for calculating λ_g (in nm) listed in Table 1, are shown in Fig. 4. In many previous publications a value of $E_g = 3.2$ eV was determined for bulk TiO₂ [3]-[8, 44].

Tab. 3. Comparison of the surface areas from BET equation, Everett-Schay function and Schay-Nagy (S-N) extrapolation method

Photocatalyst sample	Slope of Eq. (12) $= 1/n_{1,0}^s$	$n_{1,0}^s$ (mmol/g)	n_1^s (mmol/g)	a_L (m ² /g)	a_L (m ² /g)	a_{BET}^s (m ² /g)	t^s (nm)
	Calculated after Eq. (12)		From S-N extrapolation Eq.(7)	Eq(12)	From S-N extrapolation Eq.(7)		From Eq.(16)
TiO ₂ 20/MA	0.3111	3.2144	3.06	386	367	153	0.475
TiO ₂ 33/MA	0.3649	2.7405	2.67	329	320	198	0.483
TiO ₂ 50/MA	0.4380	2.2831	2.45	274	294	240	0.487
TiO ₂ 66/MA	0.5202	1.9223	2.06	231	247	251	0.535
TiO ₂ 75/MA	0.5563	1.7976	1.77	216	212	270	0.491
Sol-gel TiO ₂	0.6744	1.4828	1.53	178	183	268	0.515
Na-montm.	0.5320	1.8797	1.92	225	230	47	0.512

Cross section area of ethanol: $A_m = 120 \text{ m}^2/\text{mmol}$

Tab. 4. Photocatalytic characterization of the samples

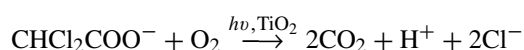
Sample	TiO ₂ content	0.01 M KOH consumption % (ml)	produced H ⁺ (mmol) after 60 min	produced H ⁺ /g catalyst (mmol/g)	produced H ⁺ /g TiO ₂ (mmol/g)	Conversion after 60 min irradiation (%)
sol-gel TiO ₂	100	10.95	0.1221	0.6105	0.6105	63.06
TiO ₂ 75/MA	69.0	3.59	0.0389	0.1945	0.2818	20.85
TiO ₂ 66/MA	63.5	3.56	0.0387	0.1935	0.3047	20.76
TiO ₂ 50/MA	47.4	2.21	0.0260	0.1297	0.2743	13.93
TiO ₂ 33/MA	29.4	2.11	0.0235	0.1175	0.3994	12.66
TiO ₂ 20/MA	18.9	0	0	0	0	0
Na-montm.	0	0	0	0	—	0
direct photolysis	0	0	0	0	0	0

The Table 1 also reveals that the value of E_g for calcinated sol-gel TiO₂ is further decreased, which can be explained by an increase in the extent of crystallinity and in particle size of TiO₂. The optical properties of TiO₂ nanoparticles on the acid-treated support are closer to those of pure TiO₂ prepared by the sol-gel method.

Table 3 compares the solid-gas and solid-liquid adsorption data. The specific surface areas calculated with the two different methods agree well with each other. The liquid sorption isotherms show different slopes because the adsorption capacities calculated for the preferentially adsorbed polar component ethanol increase with the free interlamellar space of TiO₂-montmorillonite photocatalyst. This interlamellar adsorption space is responsible for the accessibility of adsorbed DCA molecules for photocatalytic decomposition (see Fig. 5).

3.2 Photocatalytic properties

The photocatalytic efficiency of TiO₂-containing nanocomposites was tested in the degradation of dichloroacetic acid (DCA). The reaction of DCA in the presence of UV light and catalyst is the following:



The amount of acid generated by the photocatalytic reaction can be monitored continuously by detecting the change in pH. The

results can be represented in degradation curves such as shown in Fig. 6 (initial values are taken as 100%). The figure displays the results obtained with the sample series TiO₂ /MA and with direct photolysis. In Table 4 the numerical values of degradation data are listed, namely the amount of alkali solution added, the amount of acid formed (in mmol), the amount of acid formed normalized to catalyst amount and to net TiO₂ content and conversion.

An increase in the absolute value of catalytic activity with increasing TiO₂ content can be observed. In spite of the fact that the absolute value of efficiency does indeed increase with increasing TiO₂ content of the catalysts used, a different picture emerges when the results are normalized with respect to pure TiO₂. When the catalytic efficiency is normalized to the mass of the TiO₂ content, different results are obtained. The calculated data are presented in Table 4; the data of series TiO₂/MA are represented in Fig. 7. When the rate of degradation is normalized with respect to the mass of TiO₂ it is can be seen that the highest efficiencies (0.3994 mmol H⁺/gTiO₂) are attained by catalyst TiO₂ 33/M. Comparing the rate of photo-oxidation with the liquid adsorption data, the highest specific surface area (320 m²/g) of composite catalyst for liquid sorption is given for this sample, because the accessibility for DCA molecules is also highly favourable in this confined adsorption space (see Table 3).

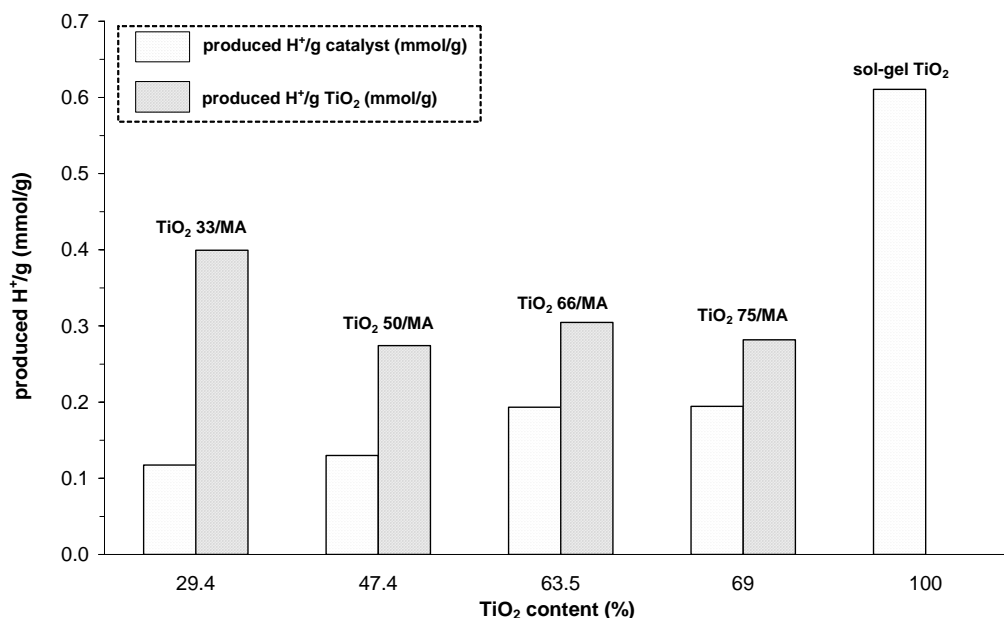


Fig. 7. Comparison of the different photocatalyst samples for DCA decomposition, calculated for pure TiO₂ and catalyst amount respectively.

4 Conclusion

The calculated structural and adsorption characteristics of TiO₂/layer silicate nanocomposites were compared to the low temperature nitrogen adsorption and ethanol-cyclohexane liquid mixture adsorption data. Gas adsorption shows greater access to the intercalated TiO₂ nanoparticles incorporated between the silicate layers. The rates of photocatalytic oxidation of the DCA molecules are correlated to the interfacial layer properties in the confined space deduced from the liquid sorption experimental data.

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